

Measuring void content with GPR

Current test with PaveScan and a comparison
with traditional GPR systems



Hålrum med GPR

SBUF-projekt pågår för att utvärdera
möjligheterna att ersätta
provkroppstestning av hålrumshalt
med oförstörande GPR-teknik

Användbar både som
produktionskontroll och vid
slutbesiktning

Tester utförda 2017 och 2018,
pilotprojekt under 2019 där
utvärderingsmetoden testas

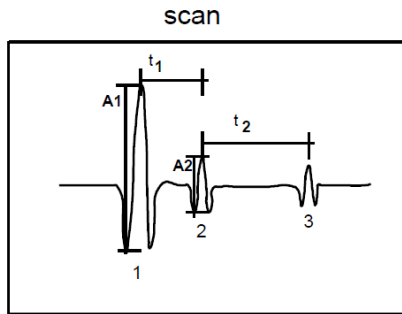
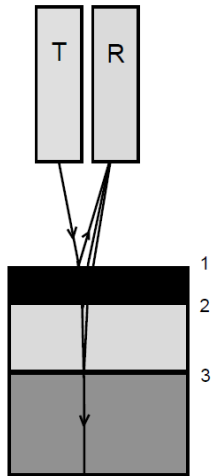


GSSI PaveScan

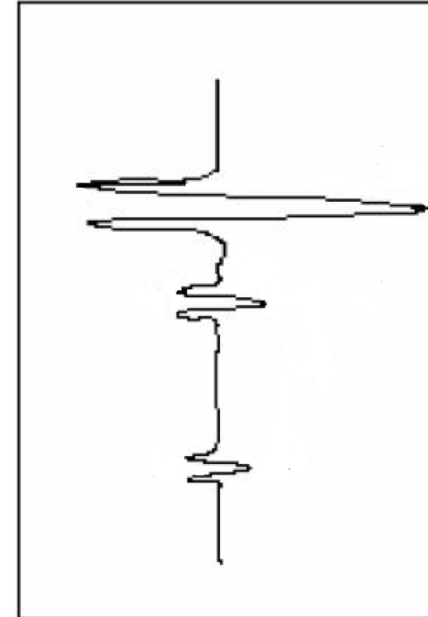


GPR Theory (the short short version)

Horn Antenna Pair



t_1 = travel time in pavement
 t_2 = travel time in base
 A_1 = amplitude of reflection from asphalt
 A_2 = amplitude of reflection from base



$$\sqrt{\epsilon} = \frac{1 + \frac{A_0}{A_m}}{1 - \frac{A_0}{A_m}}$$

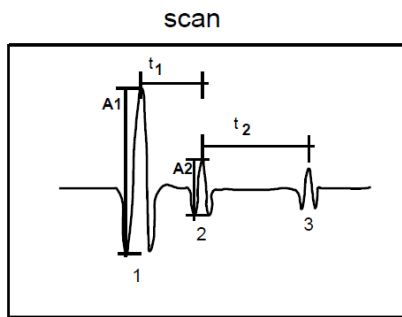
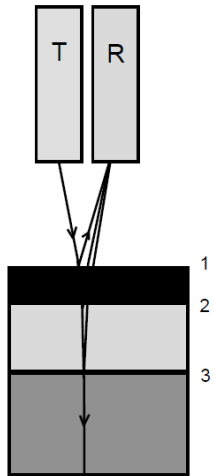
$$h = \frac{\tau \cdot c}{2 \cdot \sqrt{\epsilon_r}}$$

c = the speed of light in vacuum (0.3 m/ns)
 τ = the pulse length (ns)
 ϵ_r = medium's relative dielectricity

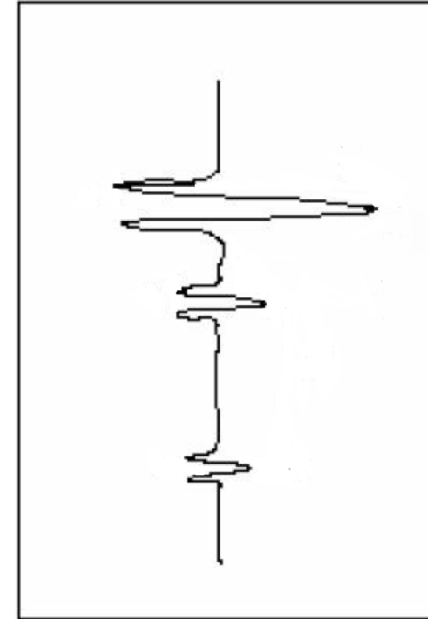
“The vertical resolution is roughly half the wave length of the pulse, which in turn is dependent on the relative permittivity of the material”

GPR Theory (the short short version)

Horn Antenna Pair



t_1 = travel time in pavement
 t_2 = travel time in base
 A_1 = amplitude of reflection from asphalt
 A_2 = amplitude of reflection from base



$$\sqrt{\epsilon} = \frac{1 + \frac{A_0}{A_m}}{1 - \frac{A_0}{A_m}}$$

$$K_{(i)} = \frac{\ln 272.93 - \ln H_{(i)}}{1,3012 \cdot X_{(i)}}$$

där $\begin{cases} H_{(i)} = \text{Hålrums halt, referensprov} \\ X_{(i)} = \text{Permittivitet i referenspunkt} \end{cases}$

$$Y_{(x)} = 272.93 \cdot e^{-1,3012 \cdot K \cdot \epsilon_x}$$

där $\begin{cases} K = \text{Kalibreringskonstant enligt (6)} \\ \overline{\epsilon_x} = \text{Permittivitet, lvärde per meter enligt (5)} \end{cases}$



GSSI PaveScan



Purpose and overview

Benchmark PaveScan against other GPR systems in order to investigate differences, strengths and weaknesses



Add-on: Combine GPR data with texture data (MPD)

Test objects

- Selected by SRA, one with new asphalt and one subjected to traffic
- E20 Hova
 - Newly paved surface, not exposed to traffic (unfortunately a bit dirty)
 - 2 sections, both 573 m long
 - 3 runs on each direction
 - Right/left wheel path + middle
 - 9 static measurements + drill cores
- E20 Örebro
 - Highway exposed to one year of traffic
 - 2 sections, 10 474 m and 11 177 m
 - 1 run in each direction, right wp
 - 9 static measurements + drill cores
- Poor weather conditions



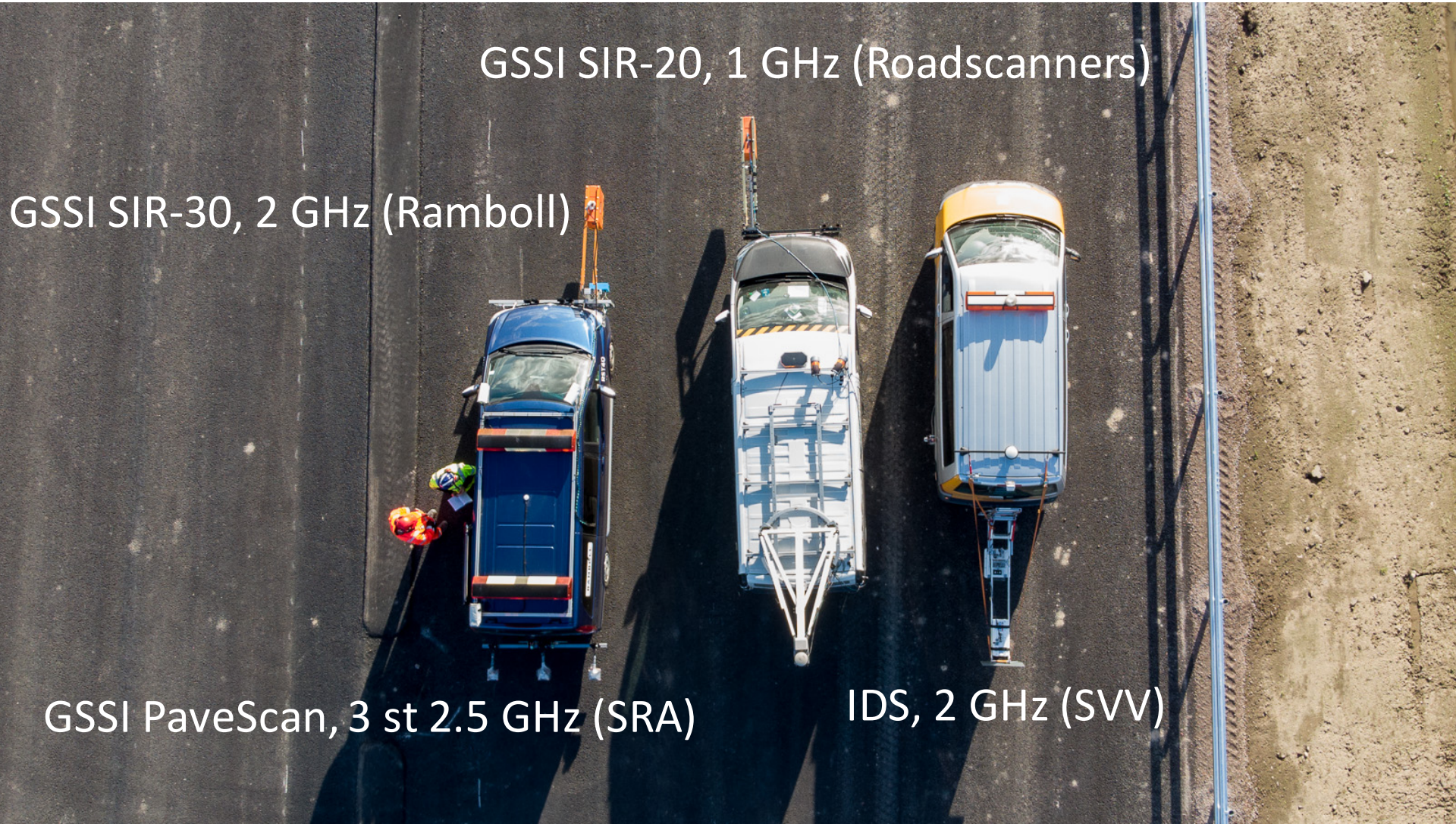
Participating systems

GSSI SIR-20, 1 GHz (Roadscanners)

GSSI SIR-30, 2 GHz (Ramboll)

GSSI PaveScan, 3 st 2.5 GHz (SRA)

IDS, 2 GHz (SVV)



Participating systems



Additional laser data from 2017 and 2018 on E20 Örebro



Laser data collected simultaneously with GPR, longitudinal profile

E20 Hova

- E20 Hova
 - Newly paved surface, not exposed to traffic (unfortunately a bit dirty)
 - 2 sections, both 573 m long
 - 3 runs on each direction
 - Right/left wheel path + middle
 - 9 static measurements + drill cores

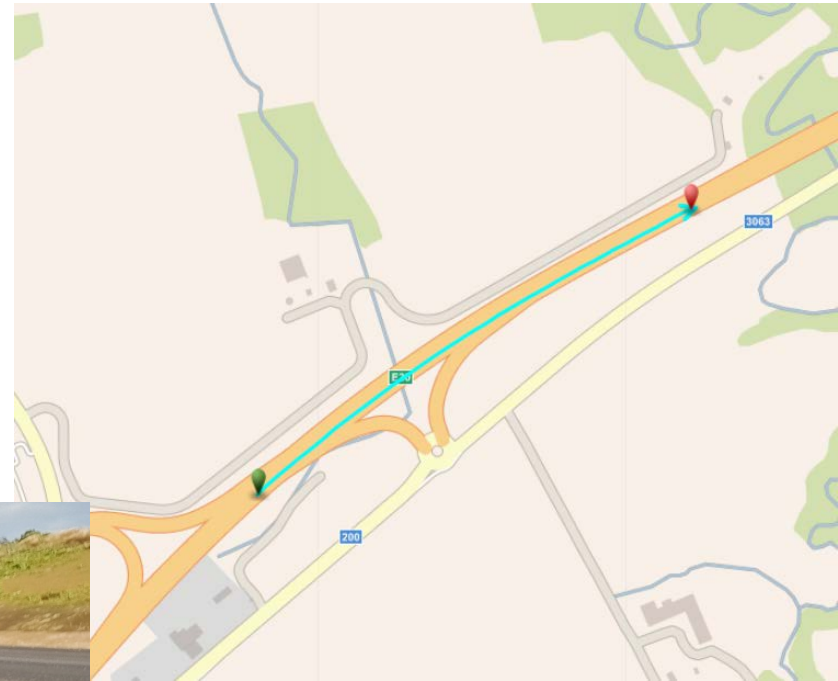


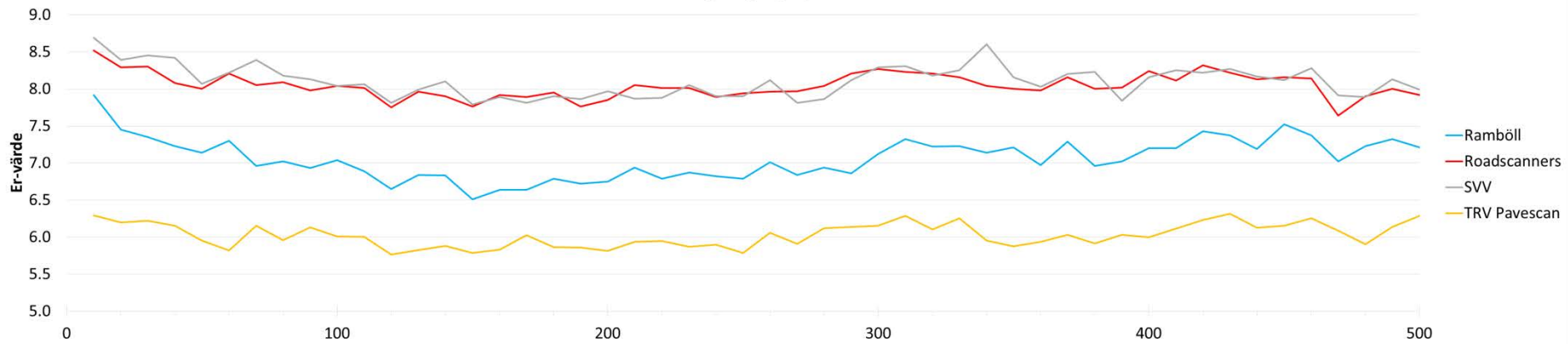
ABb22

paved 2 weeks before

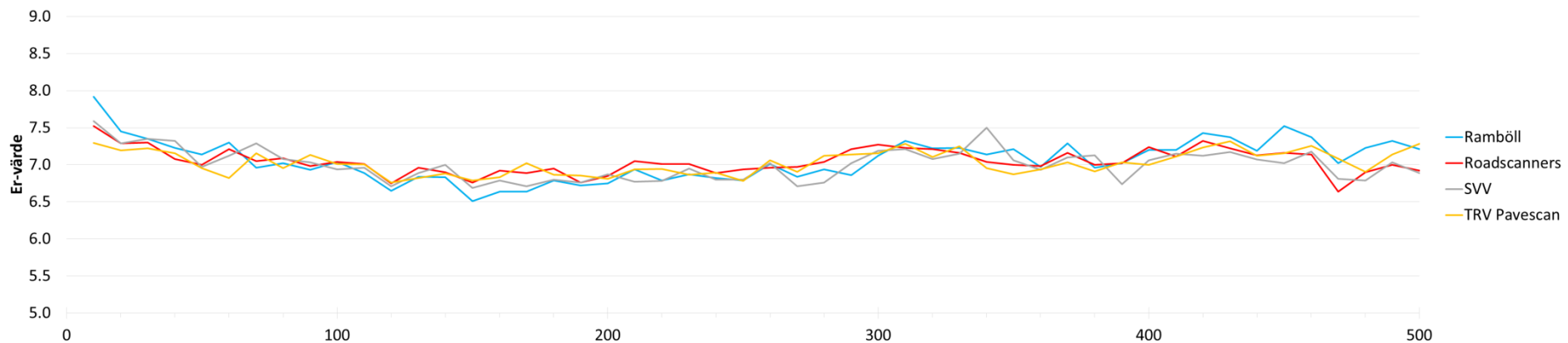
E20 Hova

- Difference in measured E_r -values between the systems, probably due to differences in signal processing and influence depth
- Normalized E_r -values show good match

Hova Norr höger hjulspår, Er-värde 10m data

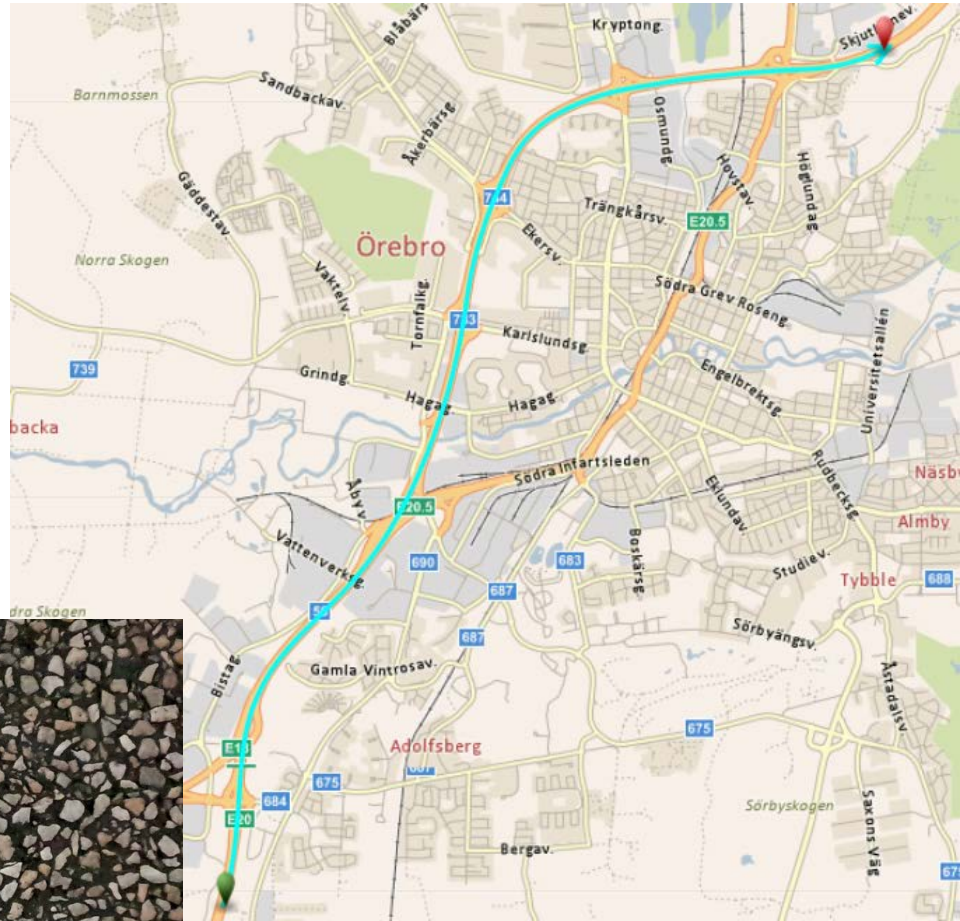


Hova Norr höger hjulspår, Normaliserade Er-värde 10m data



E20 Örebro

- E20 Örebro
 - Highway exposed to one year of traffic
 - 2 sections, 10 474 m and 11 177 m
 - 1 run in each direction, right wp
 - 9 static measurements + drill cores



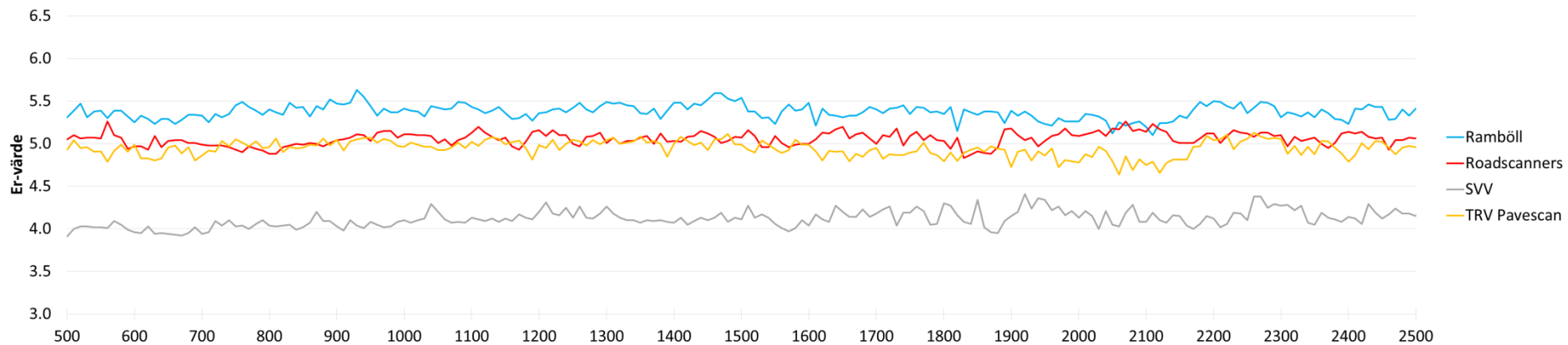
ABS16

paved june/july 2018

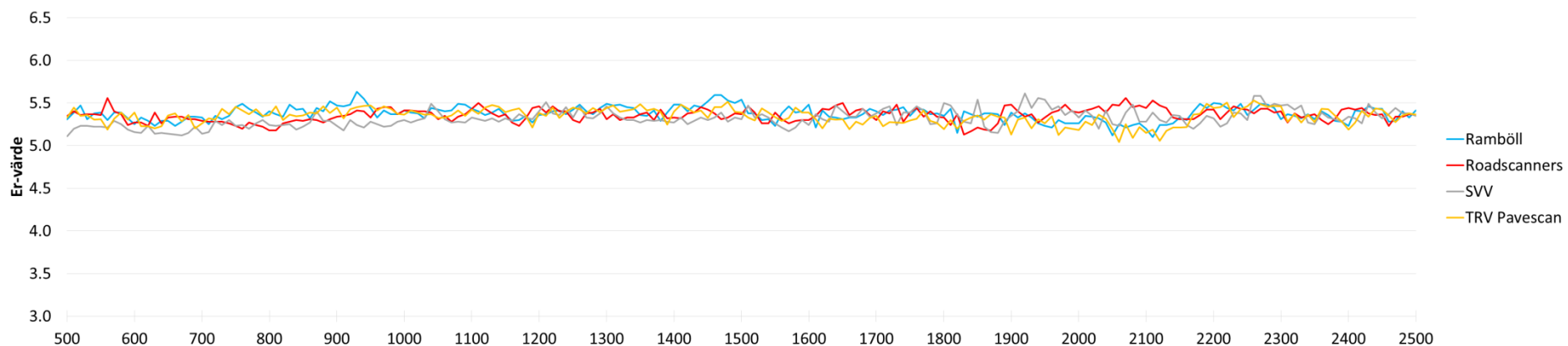
E20 Örebro

- Homogent objekt som har legat ett år sedan åtgärd
- Skillnad i mätta och beräknade absolutvärden på E_r -värde, vilket är väntat då det finns ett beroende på system, centralfrekvens och signalbearbetning
- Normaliserade E_r -värden visar på god samstämmighet (nedre diagrammet)

E20 Örebro Norr, E_r -värde 10m data



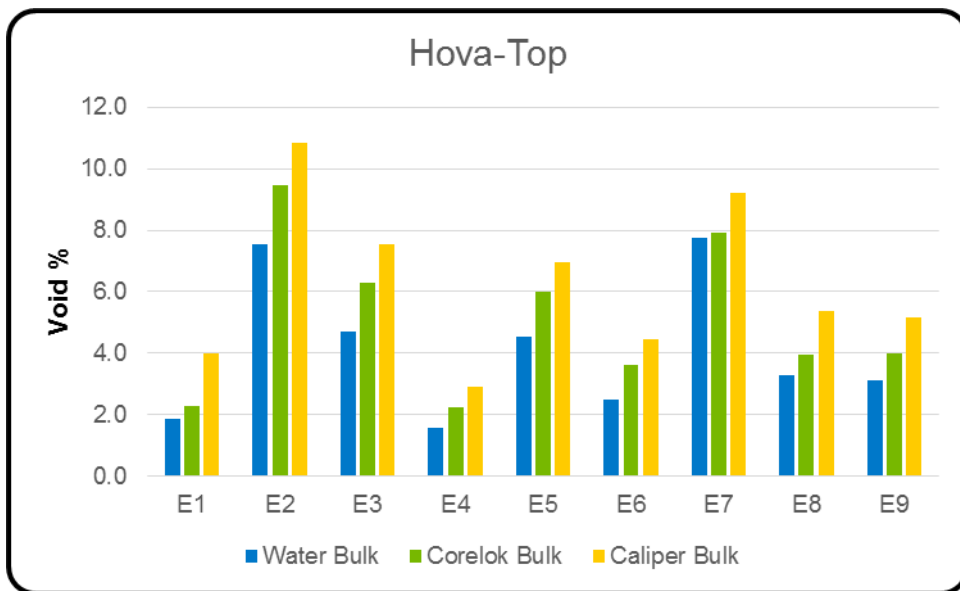
Örebro Norr, Normaliserade E_r -värde 10m data



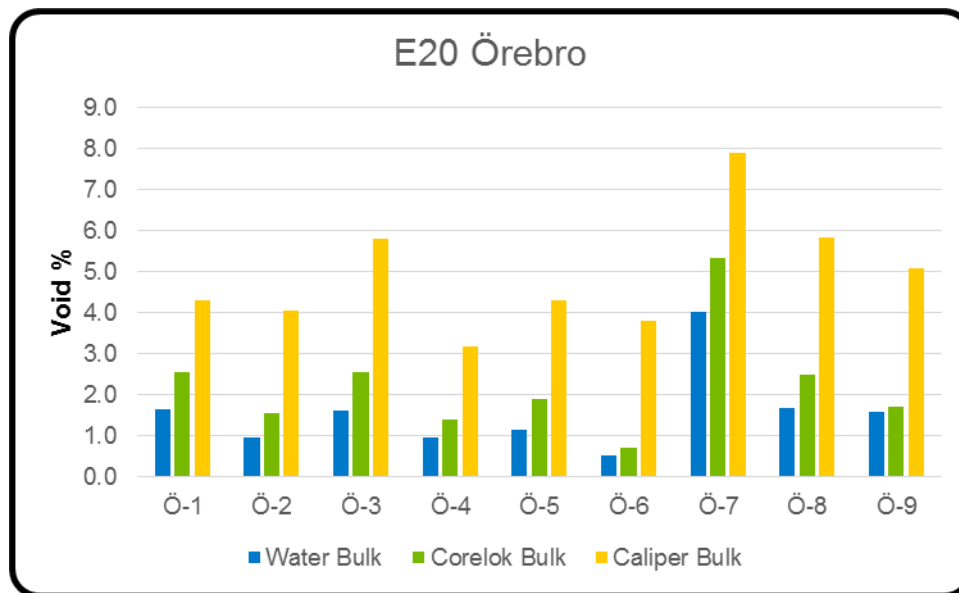
E20 Örebro



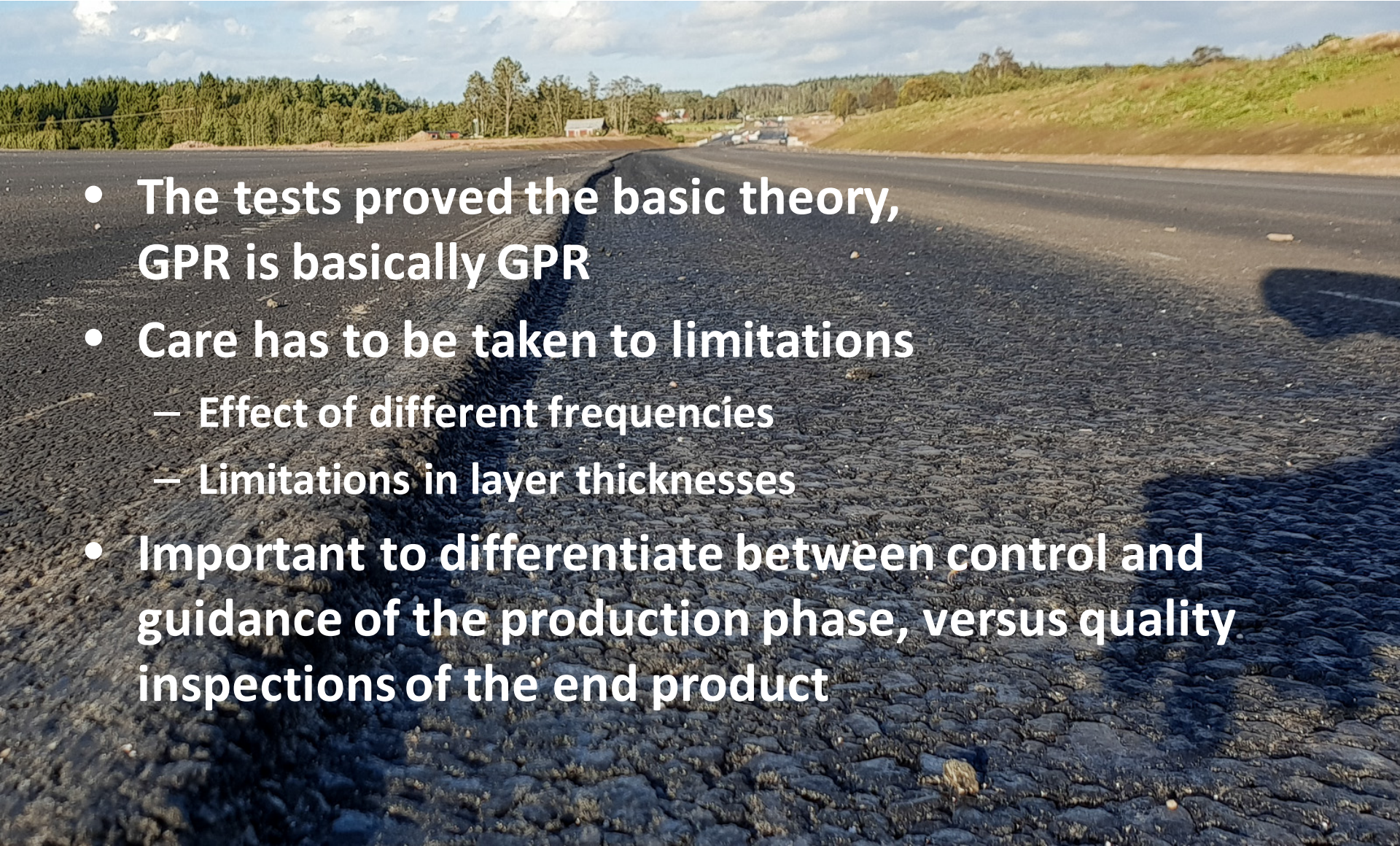
	lastrada nr:	Märkning	Thickness [mm]	Water Bulk	Void %	Corelok Bulk	Void %	Caliper Bulk	Void %	Compact
Top	11A180865	E1	65	2.641	1.9	2.630	2.3	2.584	4.0	2.691
	11A180866	E2	76	2.515	7.5	2.463	9.4	2.425	10.8	2.720
	11A180867	E3	75	2.563	4.7	2.520	6.3	2.486	7.5	2.689
	11A180868	E4	69	2.627	1.6	2.609	2.2	2.591	2.9	2.669
	11A180869	E5	68	2.587	4.5	2.548	6.0	2.522	6.9	2.710
	11A180870	E6	68	2.611	2.5	2.581	3.6	2.559	4.4	2.678
	11A180871	E7	69	2.511	7.8	2.506	7.9	2.471	9.2	2.722
	11A180872	E8	59	2.596	3.3	2.578	3.9	2.540	5.4	2.684
	11A180873	E9	65	2.609	3.1	2.585	4.0	2.554	5.2	2.693



	lastrada nr:	Märkning	Thickness [mm]	Water Bulk	Void %	Corelok Bulk	Void %	Caliper Bulk	Void %	Compact
Top	11A180912	Ö-1	36	2.379	1.7	2.357	2.6	2.315	4.3	2.419
	11A180913	Ö-2	31	2.397	1.0	2.382	1.6	2.322	4.0	2.420
	11A180914	Ö-3	37	2.395	1.6	2.372	2.5	2.293	5.8	2.434
	11A180915	Ö-4	37	2.403	0.9	2.392	1.4	2.349	3.2	2.426
	11A180916	Ö-5	39	2.387	1.2	2.369	1.9	2.311	4.3	2.415
	11A180917	Ö-6	37	2.401	0.5	2.397	0.7	2.322	3.8	2.414
	11A180918	Ö-7	39	2.346	4.0	2.314	5.3	2.251	7.9	2.444
	11A180919	Ö-8	32	2.383	1.7	2.364	2.5	2.283	5.8	2.424
	11A180920	Ö-9	34	2.378	1.6	2.375	1.7	2.293	5.1	2.416



Summary

- The tests proved the basic theory, GPR is basically GPR
 - Care has to be taken to limitations
 - Effect of different frequencies
 - Limitations in layer thicknesses
 - Important to differentiate between control and guidance of the production phase, versus quality inspections of the end product
- 

Why does the frequency matter?

“The vertical resolution is roughly half the wave length of the pulse, which in turn is dependent on the relative permittivity of the material **AND of course the frequency spectrum of the system**”

$$h = \frac{\tau \cdot c}{2 \cdot \sqrt{\epsilon_r}}$$

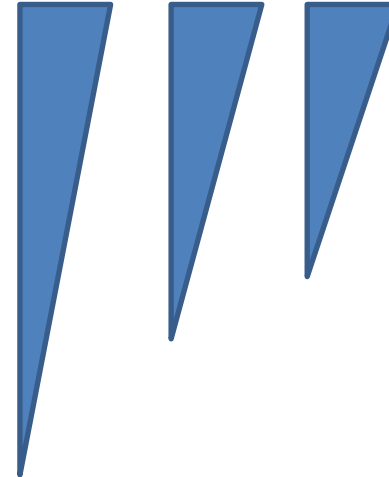
c = the speed of light in vacuum (0.3 m/ns)
 τ = the pulse length (ns)
 ϵ_r = medium's relative dielectricity



1 GHz

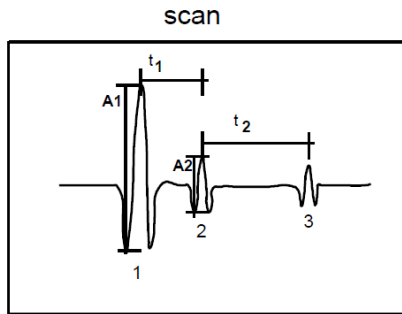
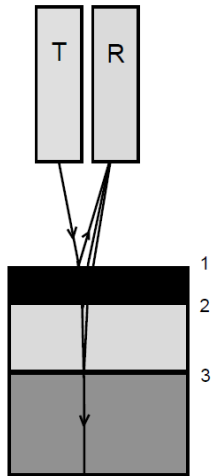
2 GHz

2.5 GHz

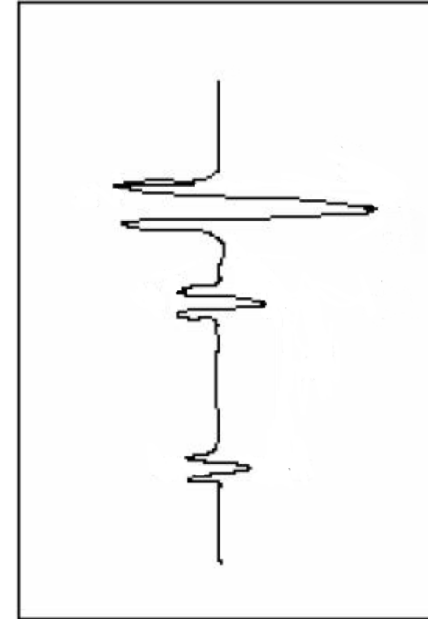


GPR Theory (the short short version)

Horn Antenna Pair



t_1 = travel time in pavement
 t_2 = travel time in base
 A_1 = amplitude of reflection from asphalt
 A_2 = amplitude of reflection from base



$$\sqrt{\epsilon} = \frac{1 + \frac{A_0}{A_m}}{1 - \frac{A_0}{A_m}}$$

$$K_{(i)} = \frac{\ln 272.93 - \ln H_{(i)}}{1,3012 \cdot X_{(i)}}$$

där $\begin{cases} H_{(i)} = \text{Hålrums halt, referensprov} \\ X_{(i)} = \text{Permittivitet i referenspunkt} \end{cases}$

$$Y_{(x)} = 272.93 \cdot e^{-1.3012 \cdot K \cdot \epsilon_x}$$

där $\begin{cases} \bar{K} = \text{Kalireringskonstant enligt (6)} \\ \bar{\epsilon}_x = \text{Permittivitet, lvärde per meter enligt (5)} \end{cases}$

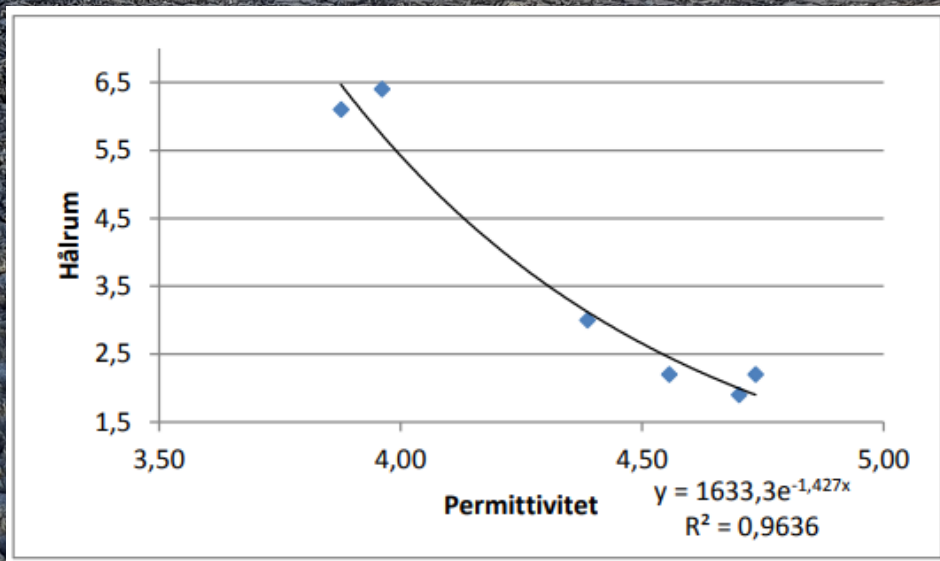
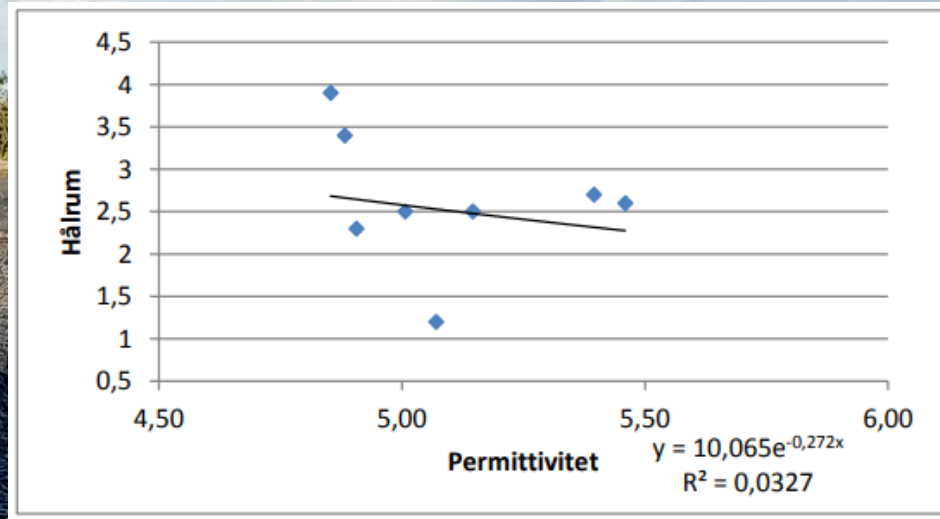
$$Y_{(x)} = \mathbf{A} \cdot e^{-\mathbf{B} \cdot \epsilon_x}$$

där $\begin{cases} \bar{K} = \text{Kalireringskonstant enligt (6)} \\ \bar{\epsilon}_x = \text{Permittivitet, lvärde per meter enligt (5)} \end{cases}$

Sammanfattning

Beläggingsobjekt	R ²
1	0,759
2	0,936
3	0,054
4	0,966
5	0,776
6	0,866
7	0,058
8	0,962
9	0,650
10	0,931
11	0,032
12	0,012

2017



Sammanfattning

Metoden fungerar, men som med de flesta metoder är utförandet väldigt viktigt

Största påverkan kommer från vattenhalten i beläggningen, det måste vara helt torrt!

Efterpackning av trafik, testning inom 2-4 veckor